

# TES Microcalorimeter Development

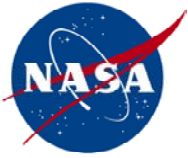
## *NIST/GSFC Collaboration*



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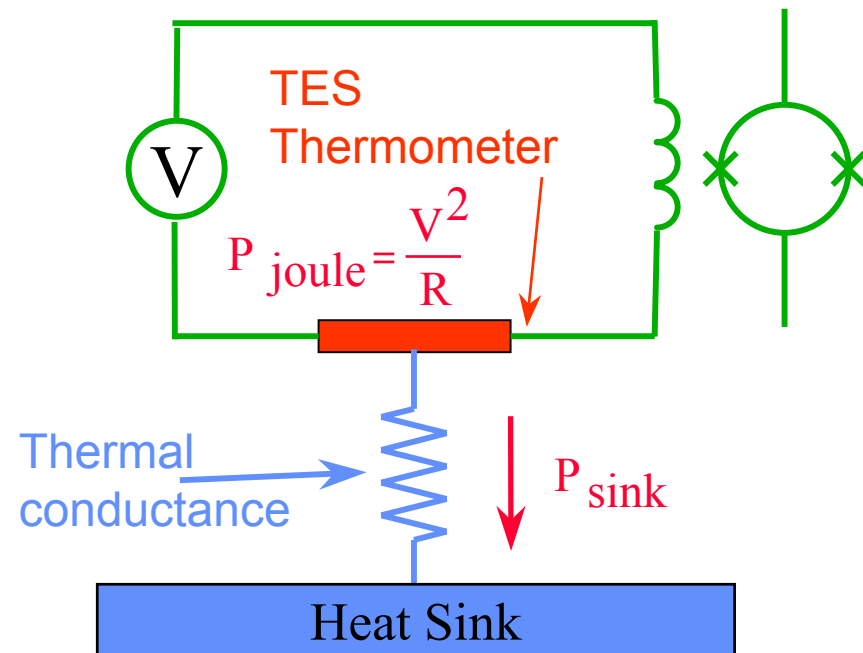
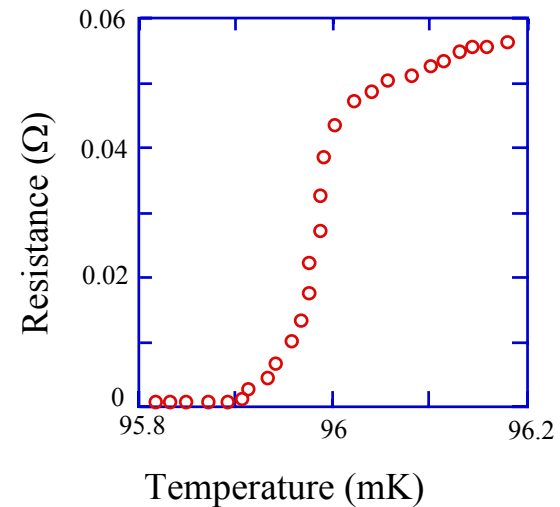
### **Outline of approach:**

- materials and process optimization
- performance optimization
- arrays and their interconnects
- SQUIDs and their multiplexers
- digital electronics



## Reminder: Operating Principles

- An x-ray calorimeter consists of a thermalizing absorber, a thermometer, and a thermal link to a low-temperature heat sink.
- In a TES calorimeter, a superconducting film self-biased between the superconducting and normal states serves as the thermometer.
- Since most superconductors undergo the transition to zero resistance at temperatures too high to be of use in a microcalorimeter, it is common to use a bilayer of normal and superconducting films to tune to a particular transition temperature.
- The choice of metals is guided by the need to survive the temperature changes and chemical exposures to which the devices will be exposed in fabrication, as well as optimizing the superconducting properties.



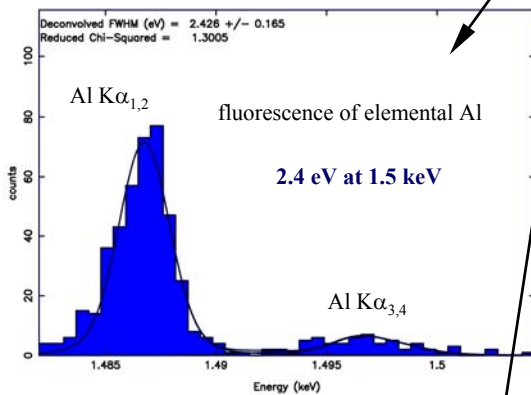


# Materials and Processes - different paths

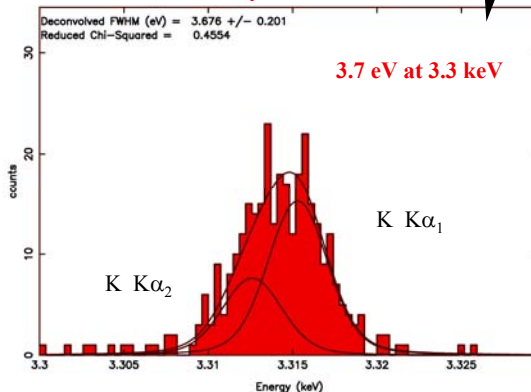


E-beam Mo/Au, Nb leads

Mo/Au TES - no x-ray absorber



Mo/Au TES - no x-ray absorber

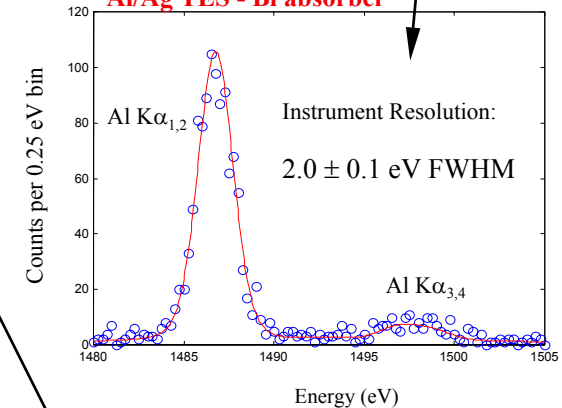


Sputtered Mo/Cu, Mo leads

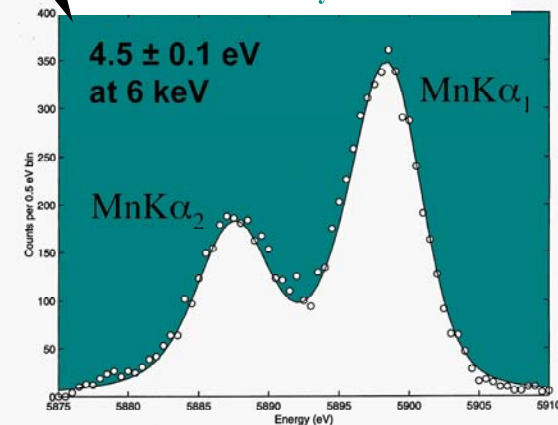
NIST has obtained good results with bilayers of Mo/Cu and Al/Ag. GSFC has done well with Mo/Au. The aluminum-based bilayers have demonstrated electrochemical corrosion, but the molybdenum-based bilayers yield robust devices.

Evaporated Al/Ag

Al/Ag TES - Bi absorber



Mo/Cu TES - no x-ray absorber



*Constellation-X*



# Materials, Processes, and Performance - Open Issues



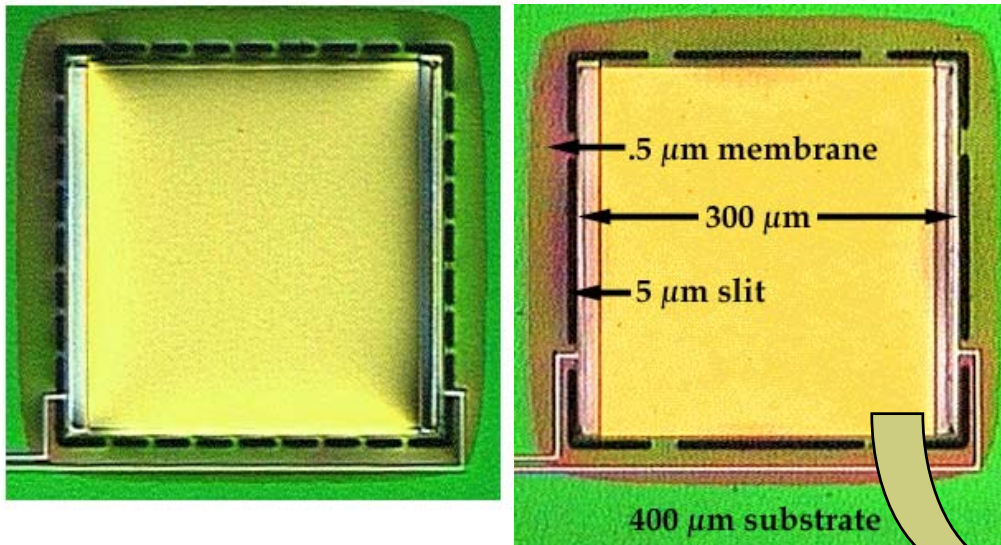
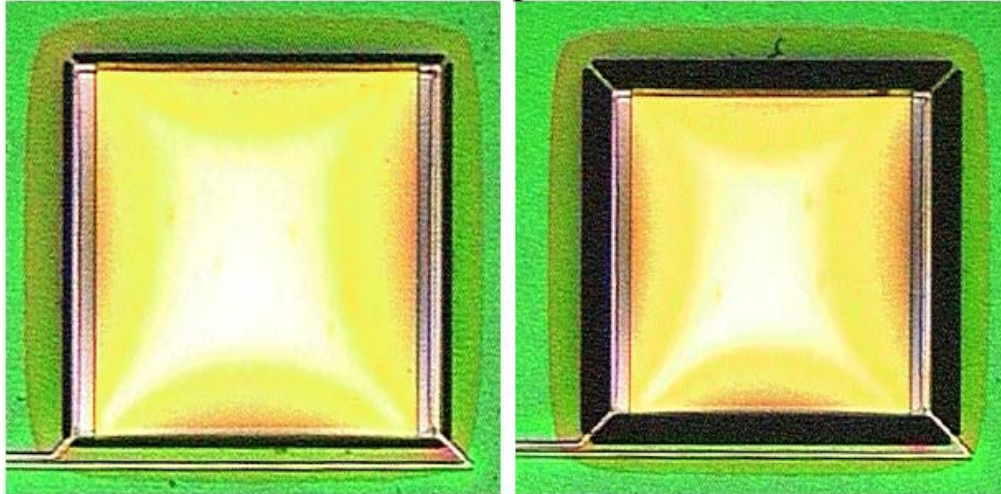
- Noise:
  - NIST and GSFC see excess noise, but with different scaling
  - need to investigate impact of materials, contacts, shape, volume, and boundary conditions (*e.g. Mo/Cu vs. Mo/Au and undercut Au boundaries vs. normal metal bars*)
  - complete main thrust of investigation in next two years
- Reproducibility:
  - new dedicated deposition system at NIST
  - ongoing  $T_c$  monitoring at GSFC
- Allocation of heat capacity between TES and absorber in Constellation-X sized pixels
- Absorbers (bismuth + Au or Cu)
  - thermalization
  - confirm no impact on underlying TES superconducting properties



## Moving to Arrays

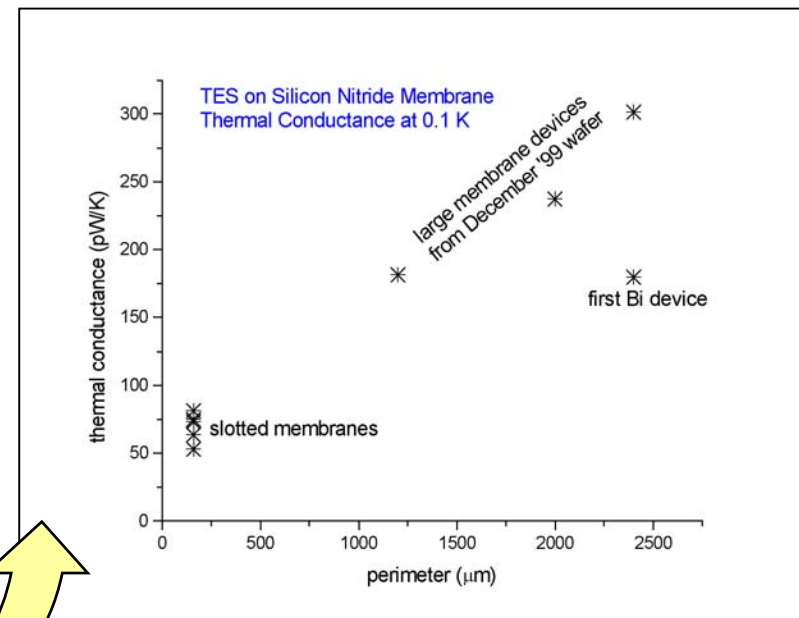


Individual TES devices designed to have different thermal conductance to allow parameterization.



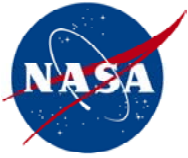
Both NIST and GSFC use silicon-nitride membranes for the thermal link.

Initially, these membranes occupied much more area than available for each pixel in the *Constellation-X* array. The present development effort at GSFC is focused on implementing compact pixels in close-packed arrays.



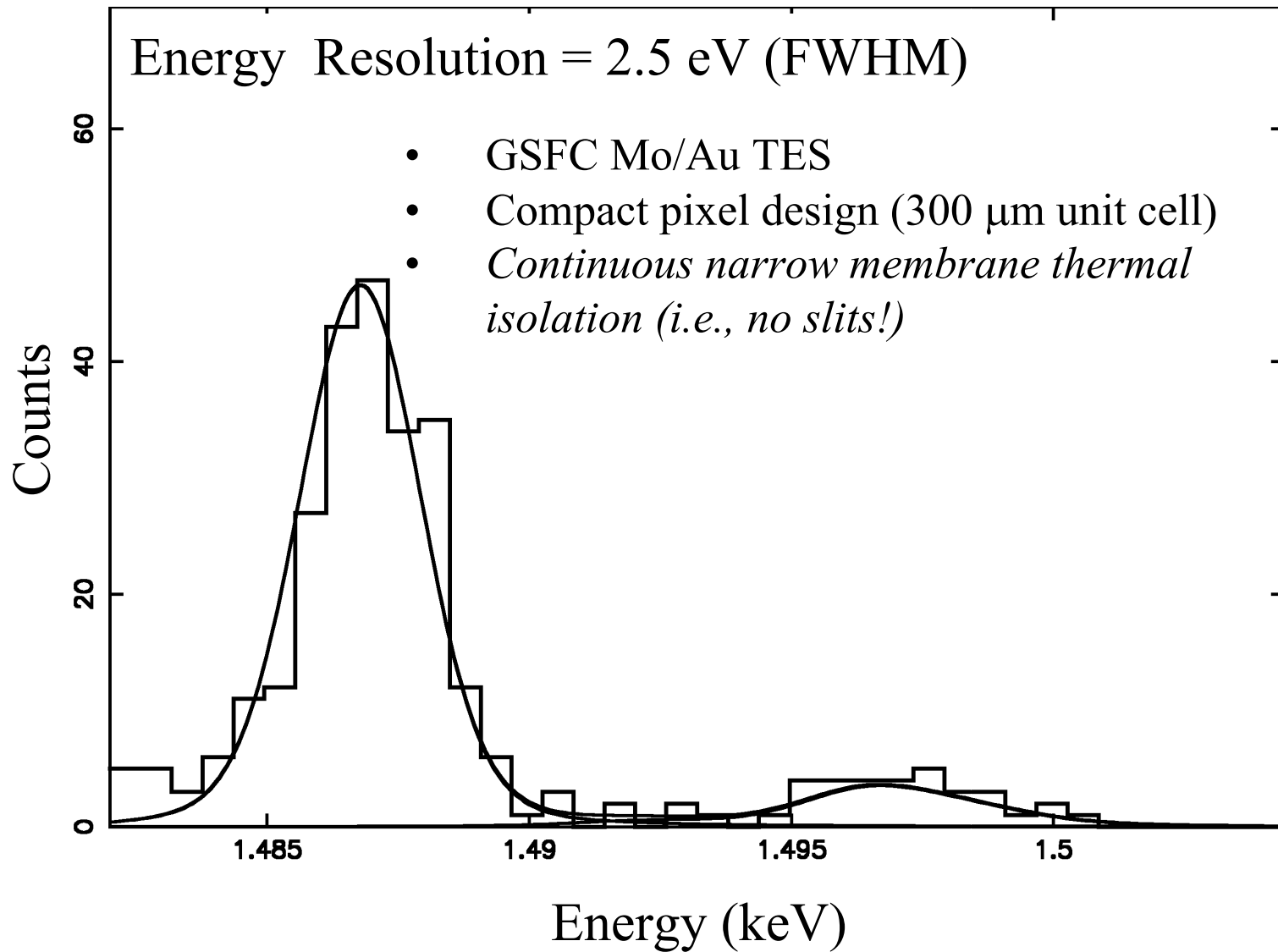
*Constellation-X*

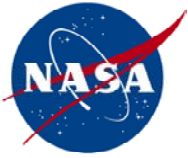




## Latest TES result...

NIST





## Compact pixel refinement



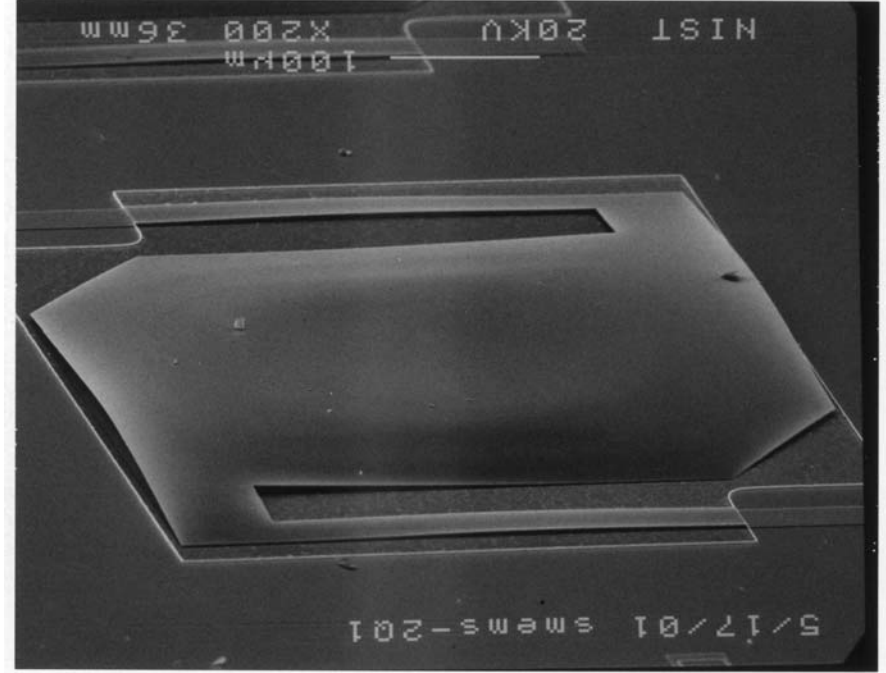
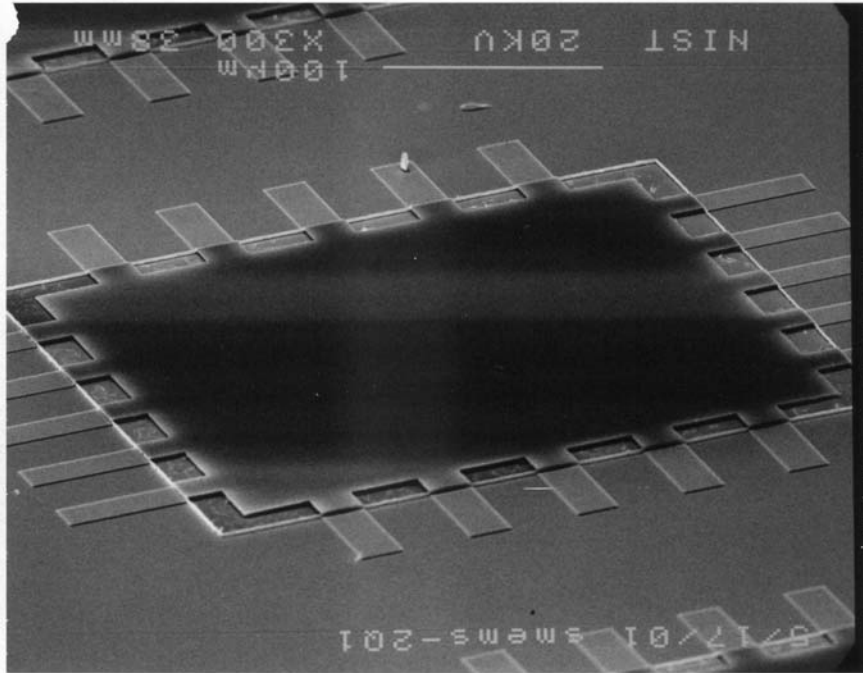
We want a robust, reliable design for the weak link, not overly sensitive to small variations in operating temperature or membrane thickness. Thus, over the next year, we will be measuring  $G(T)$  in different geometries for:

- Different nitride thicknesses (0.25, 0.5, and 1.0 microns)
- Different TES  $T_c$

At 70 mK and 0.5 microns we see evidence of phonon mode exclusion, thus extreme sensitivity to temperature and thickness is expected. We likely will have greater control with thicker membranes that have slits than with continuous thin membranes. But we need to do the measurements.

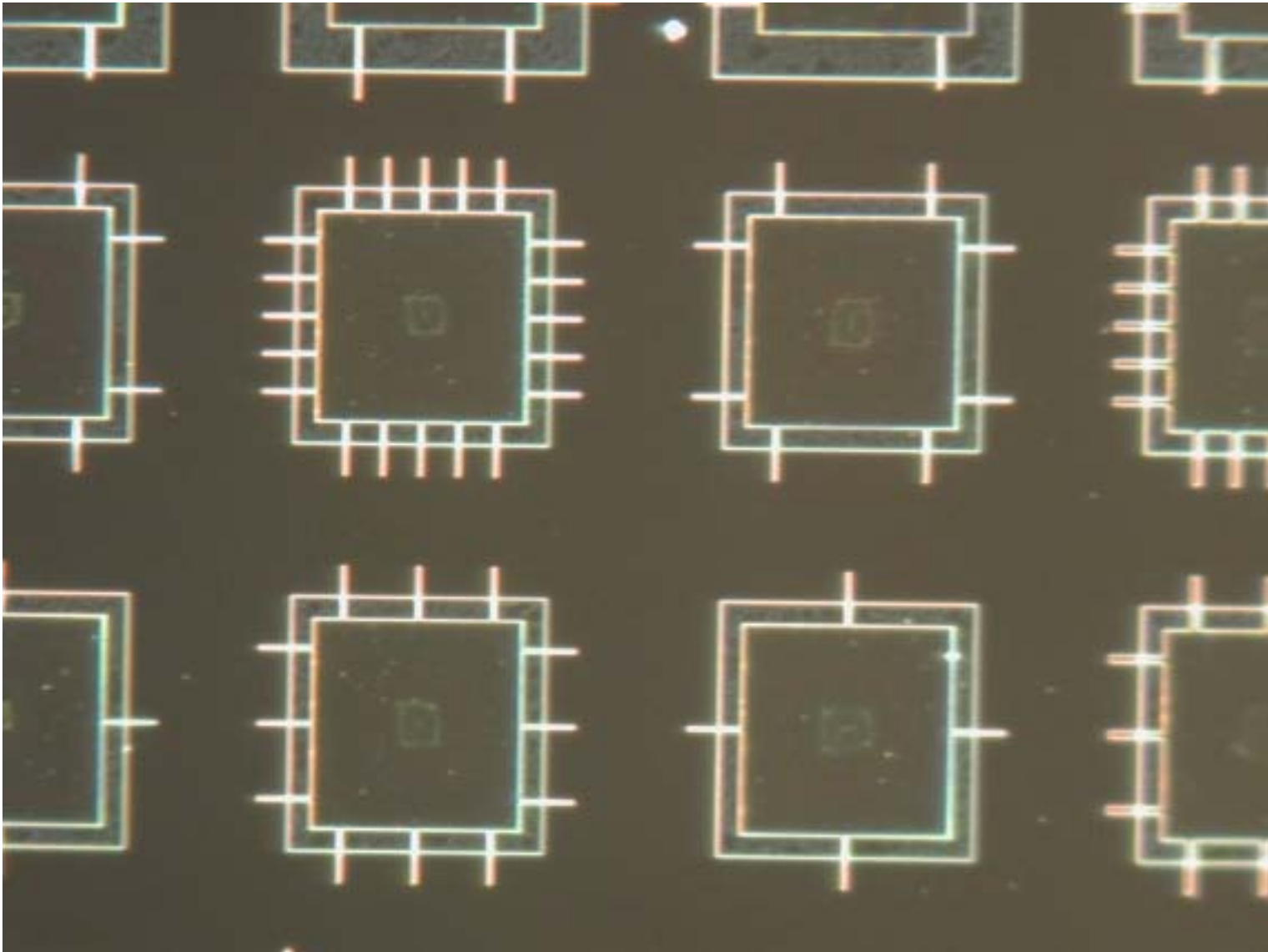


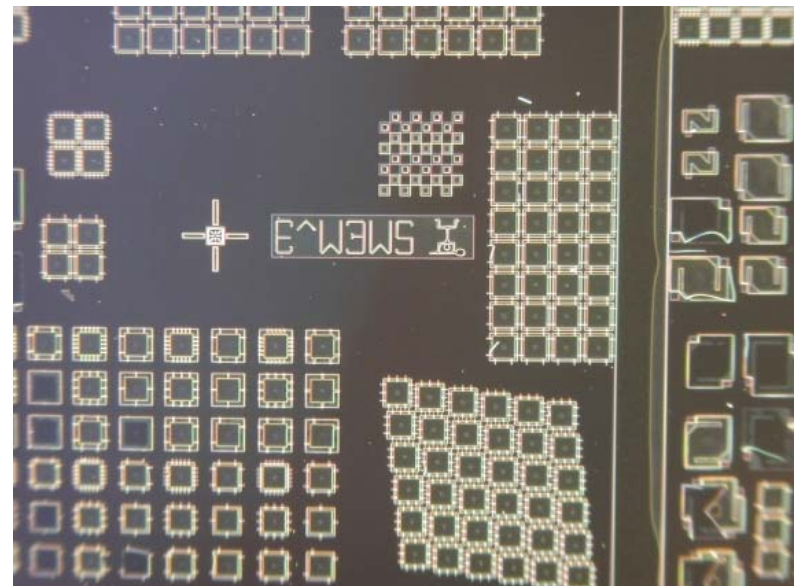
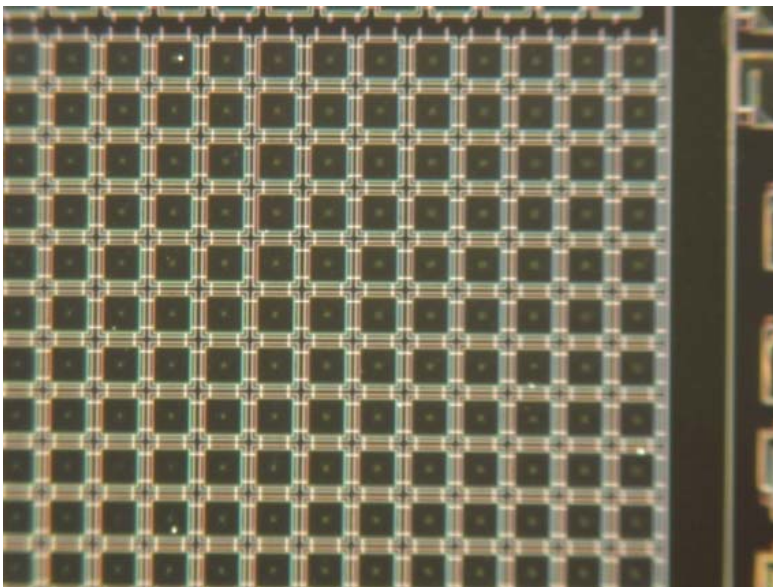
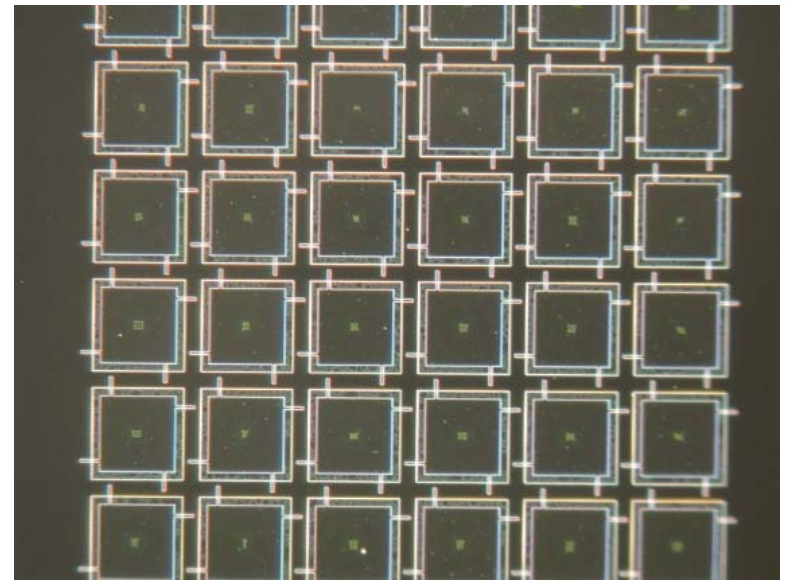
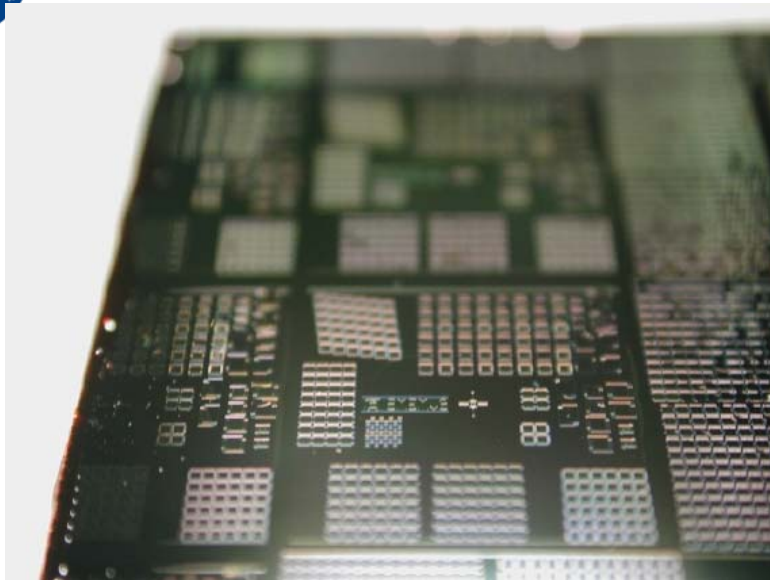
# NIST Suspended Nitride Test Structures



Nitride deposited at NIST over sacrificial polysilicon layer. Idea is to make area under the suspended devices available for wiring traces.



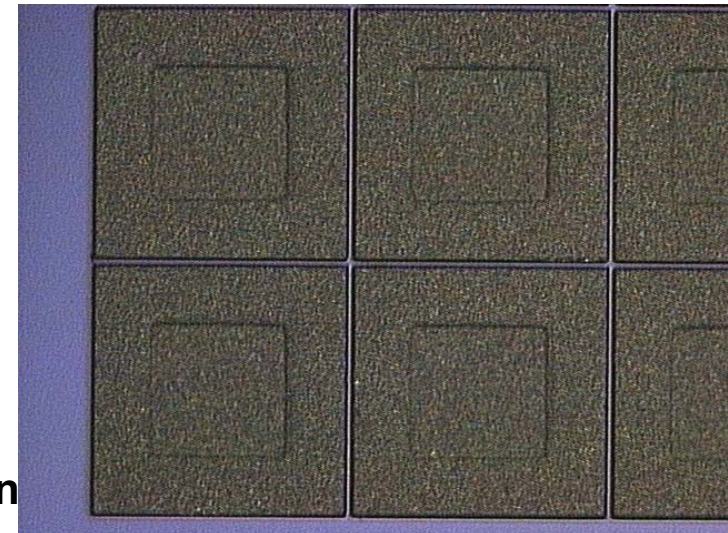
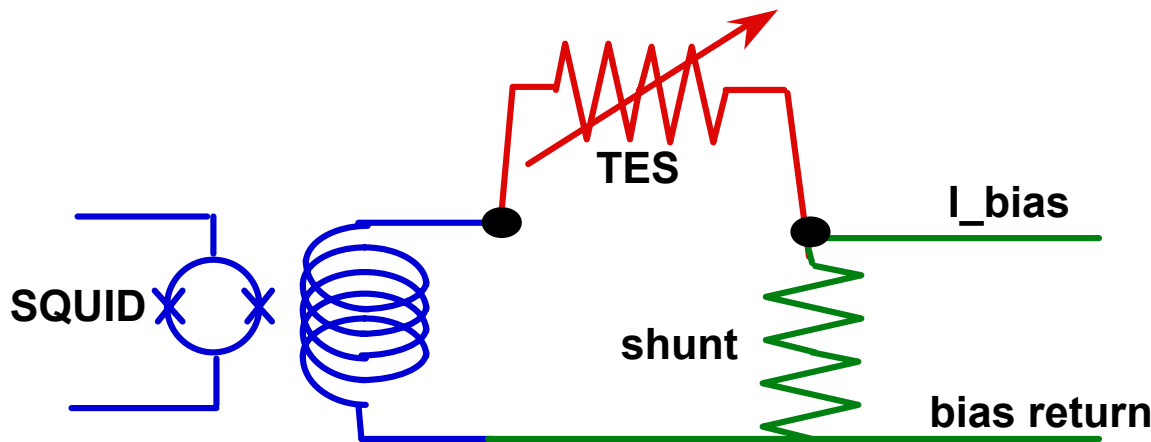
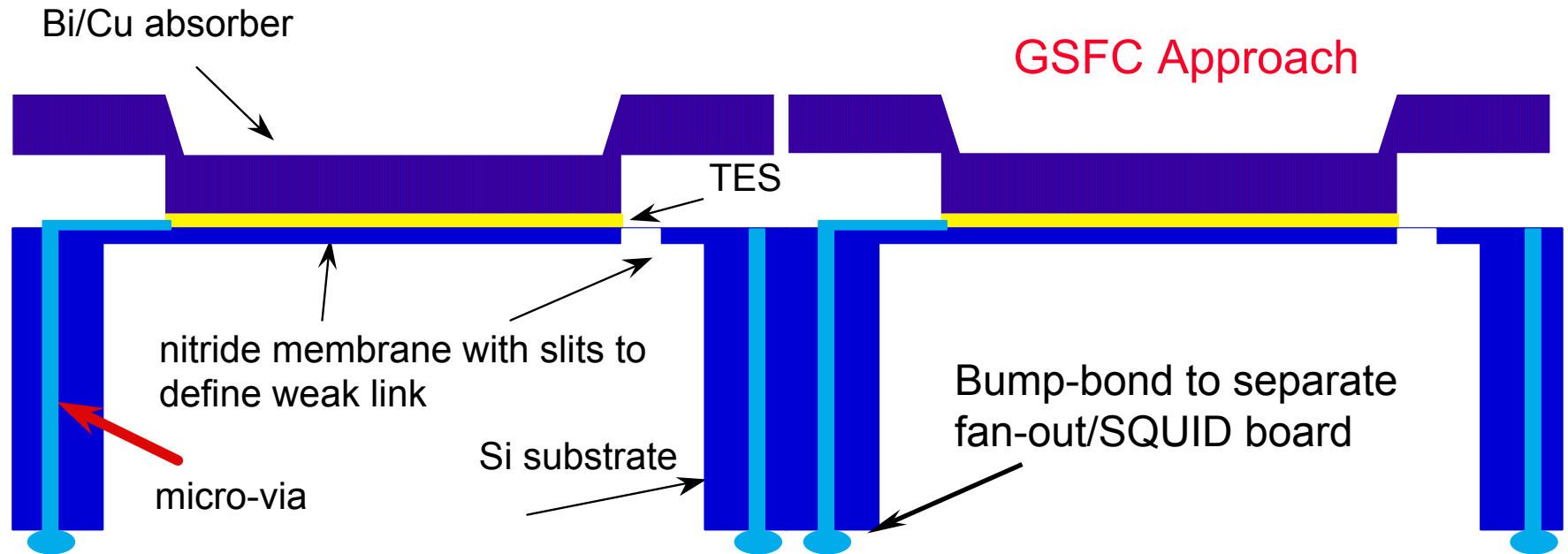




*Constellation-X*



# TES Array Concepts



*Constellation-X*

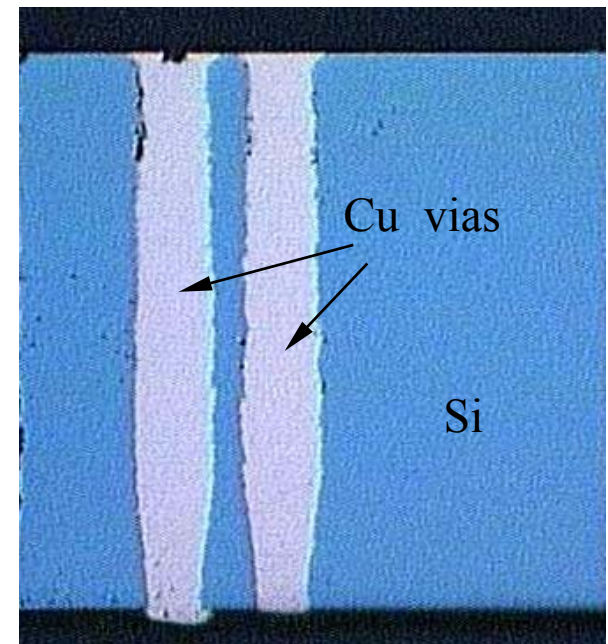
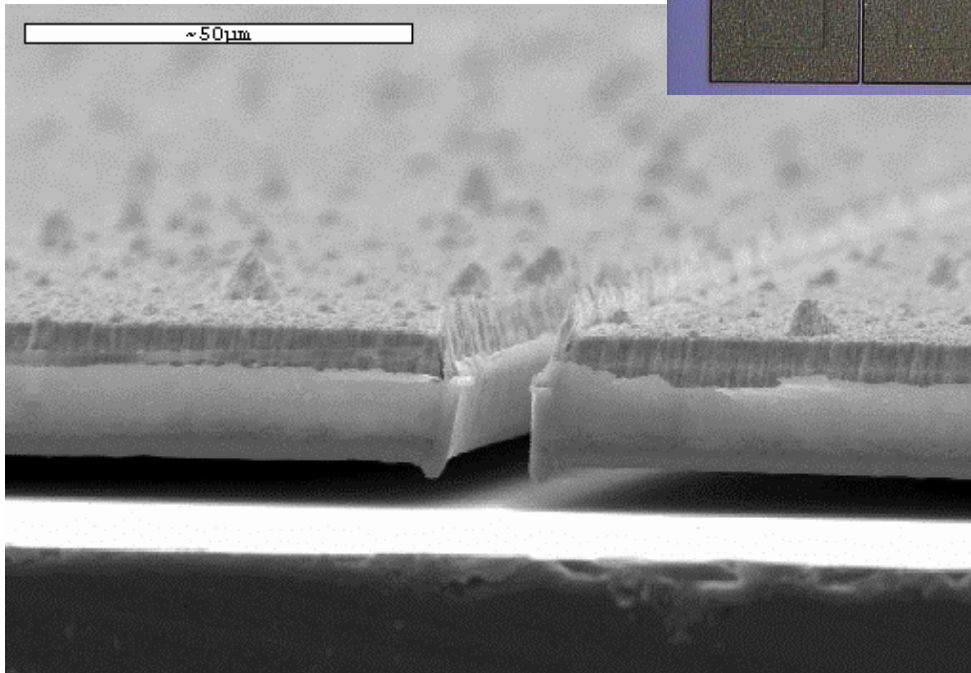
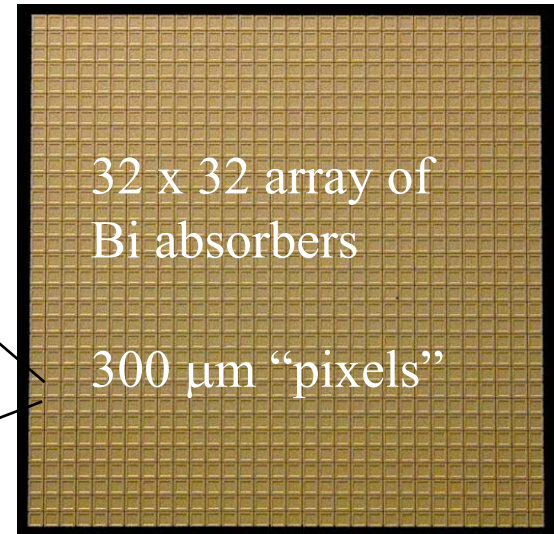
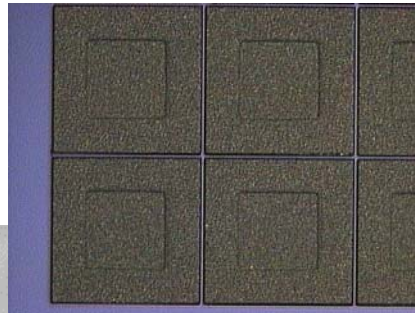


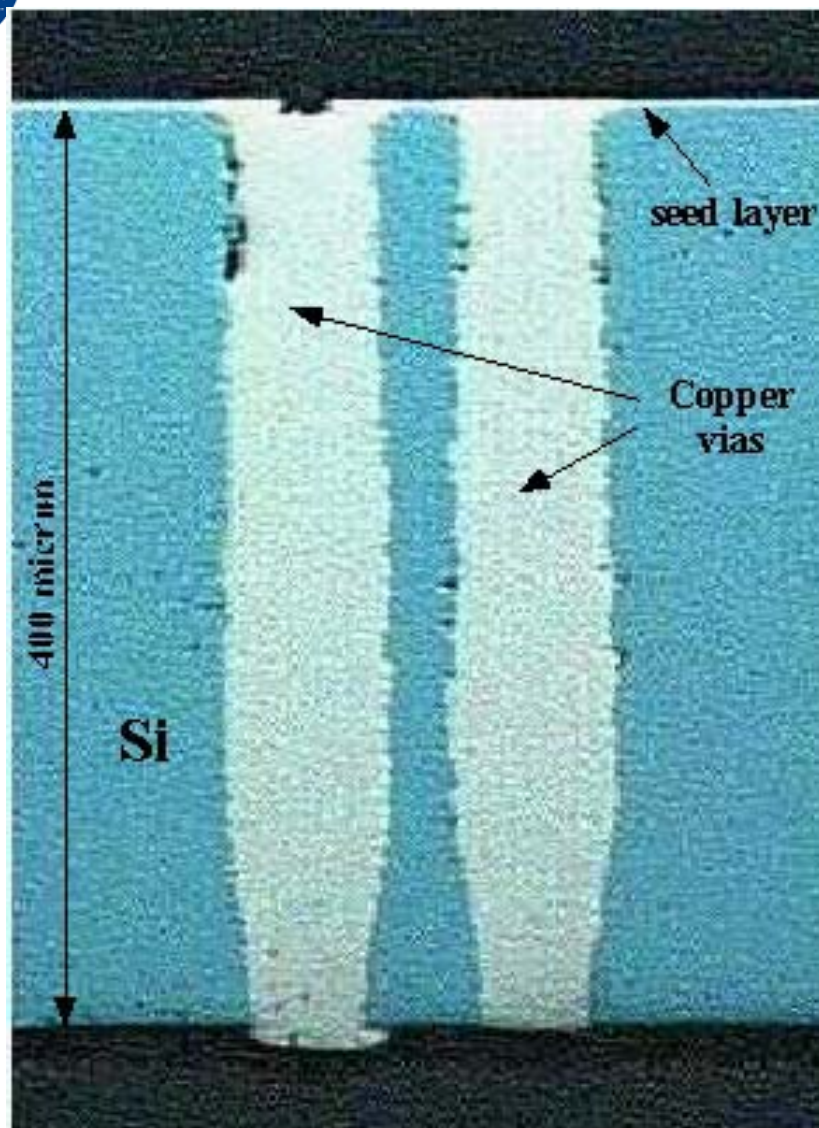


# Micromachined Bi Absorbers

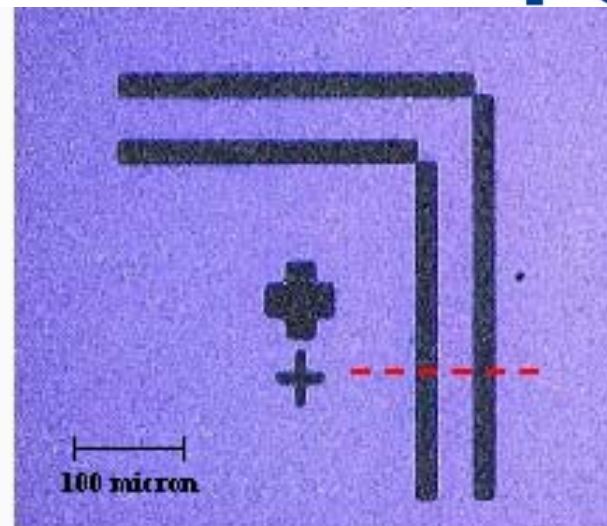


Proof of concept for  
fabricating x-ray  
absorbers in array format  
with high filling factor.

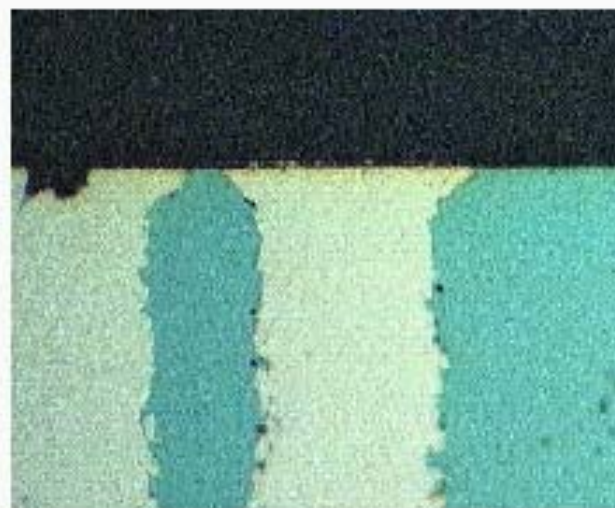




Cross-section of two copper-filled through-wafer vias. The cross-section was taken along the red dotted line in upper right photo.

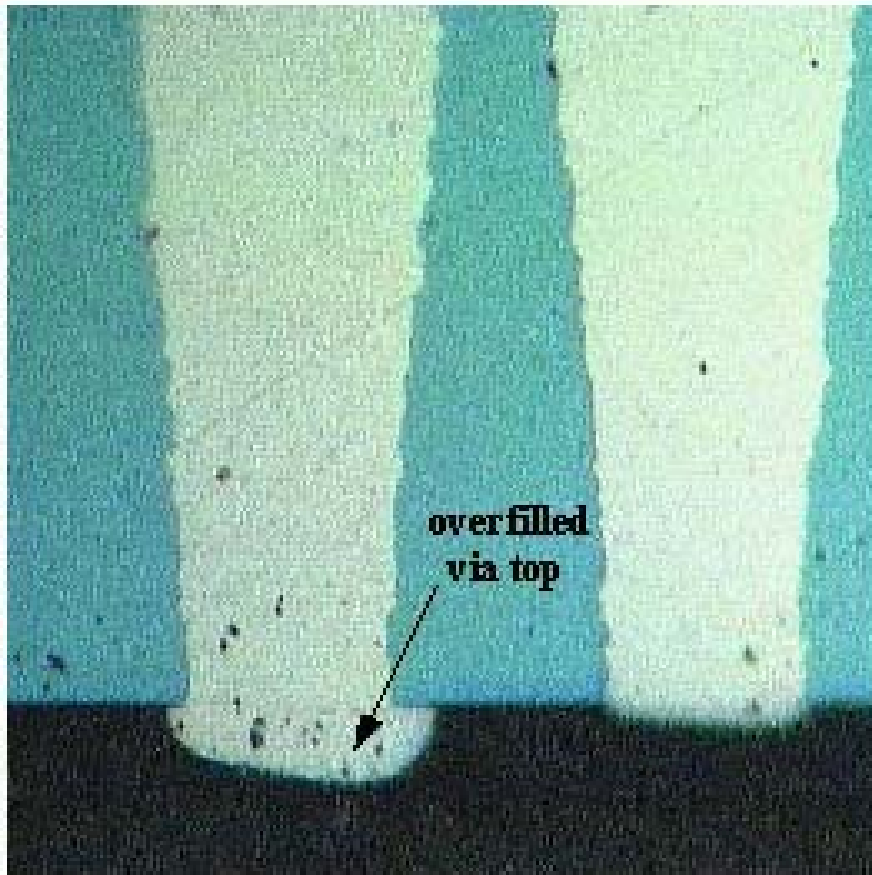


2 pairs of slotted through-wafer vias before filling them with Cu by a standard electroplating process.

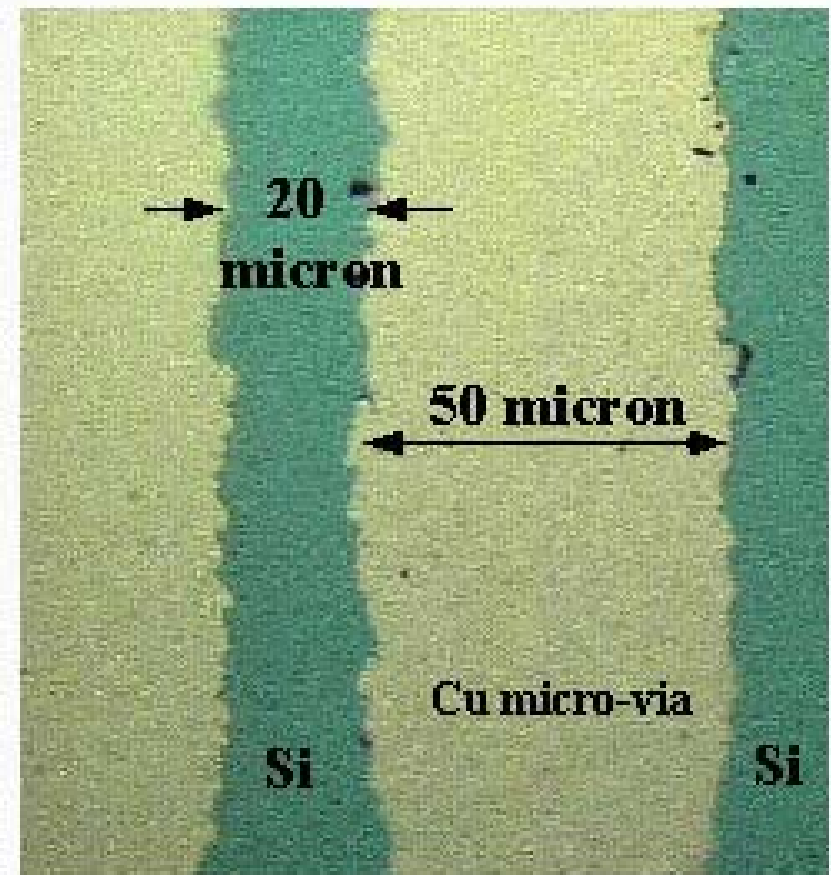


Bottom part of Cu vias after removing their Ti/Cu/Au seedlayer.

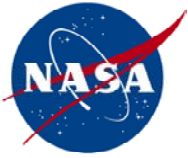




Cross-sectional view of the upper part of the two micro-vias.



Close-up on Cu micro-vias (cross-sectional view)



## Immediate TES device development plans:



### GSFC:

- Almost done with new wafer with compact pixels and higher  $T_c$  (120 mK). Half of wafer will have Bi absorbers. Dividing wafer in half along line other axis, half will have the TES boundaries defined by Au bars and half will have the boundary defined by a Mo undercut. Thus we can compare the noise of the 4 permutations, as well as get important data on thermal conductance.
- Thermally cycle vias; measure RRR

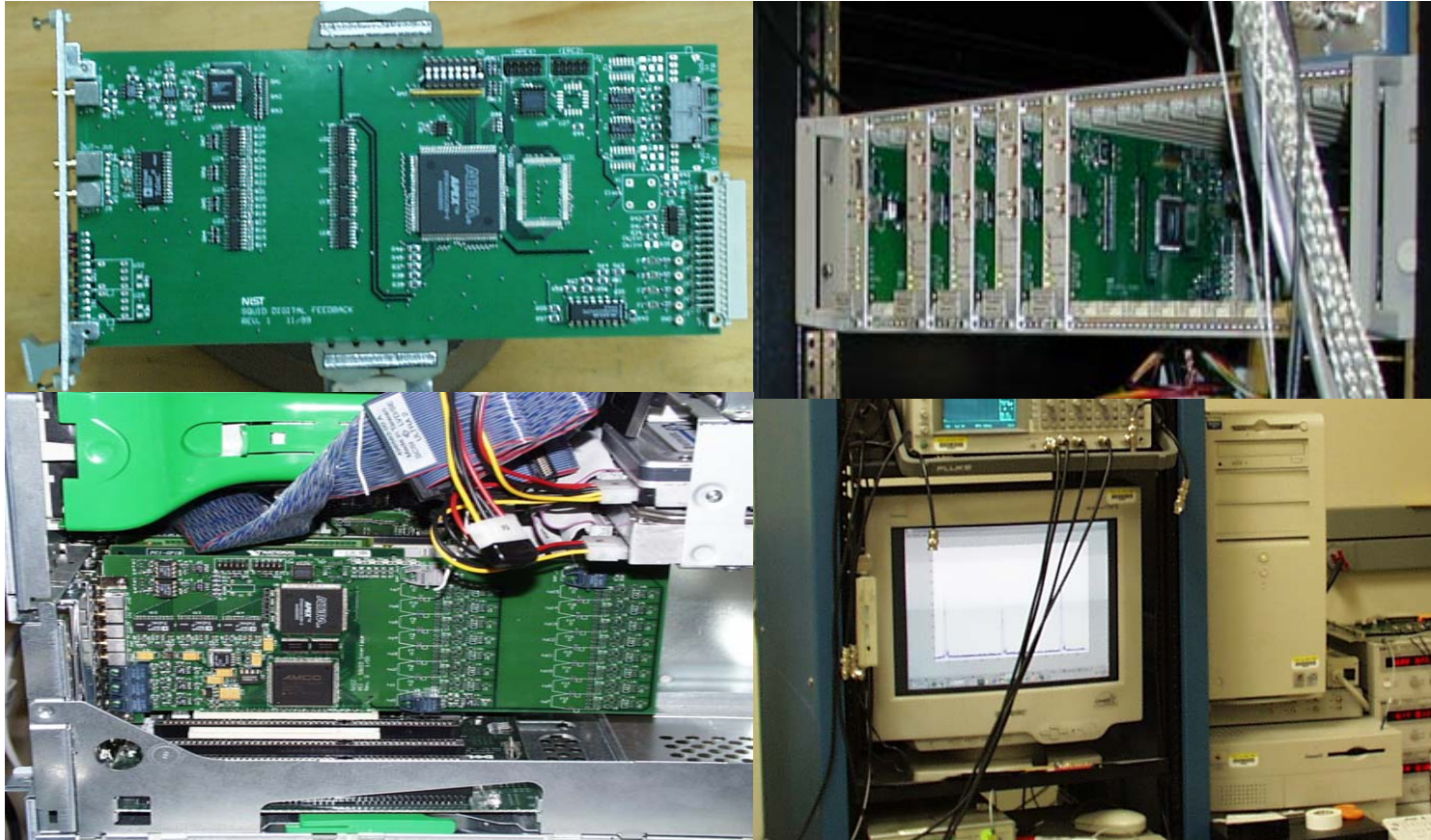
### NIST:

- Commission, start using new, dedicated deposition system.
- Perform thermal and electrical tests on surface micromachined structures.
- Fabricate prototype surface micromachined TES pixels.

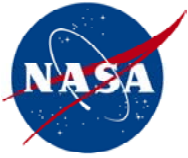




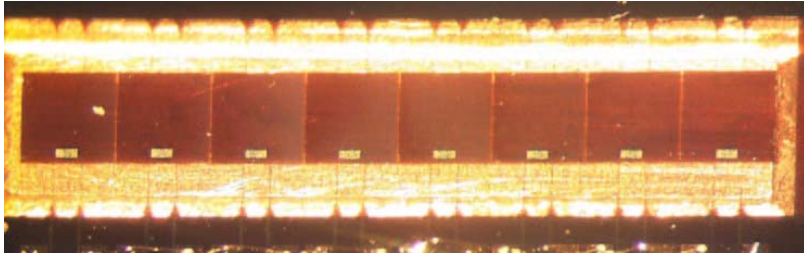
## Digital feedback electronics for TDM



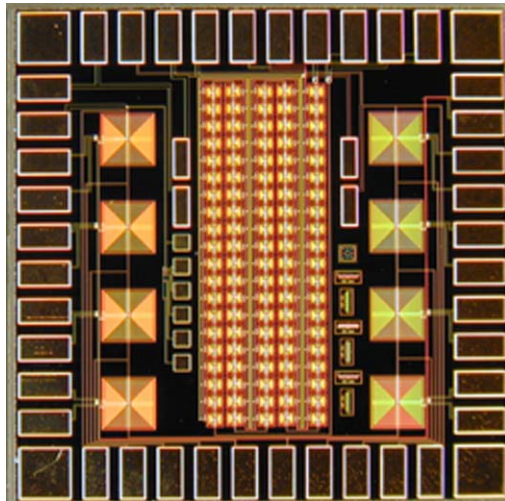




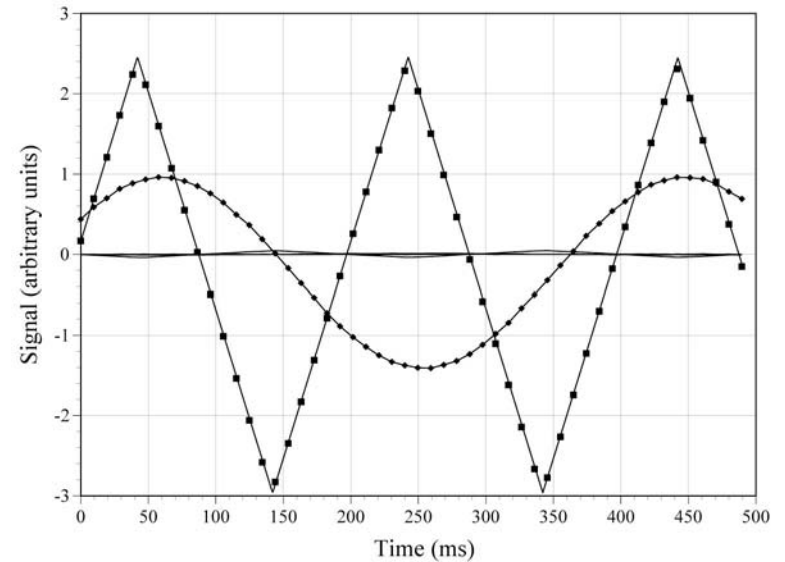
## FIBRE: a multiplexed 8-pixel TES bolometer



The TES bolometer array

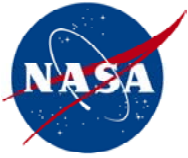


The 8-Channel TDM chip

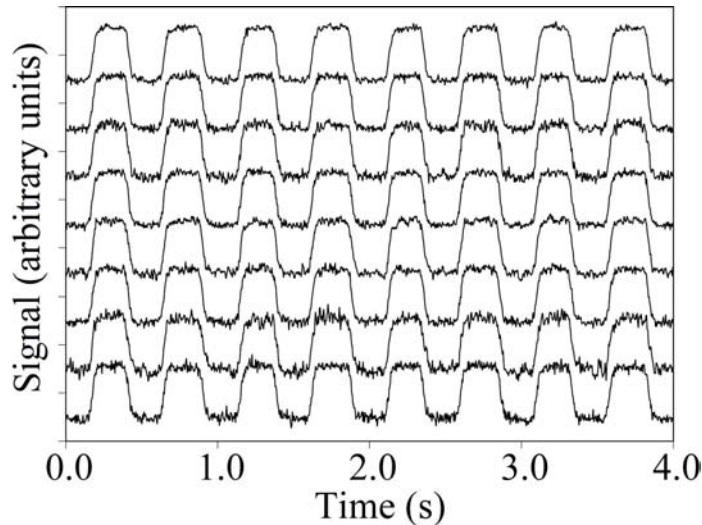


Demultiplexed readout of 8-pixel array with digital feedback and simulated signals. (One sinewave input and one triangle wave input).

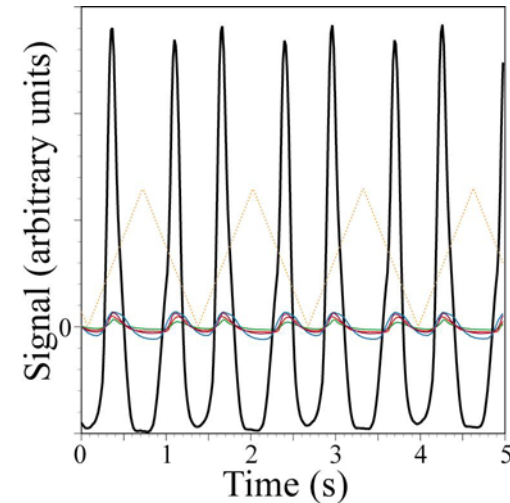




## FIBRE: optical data

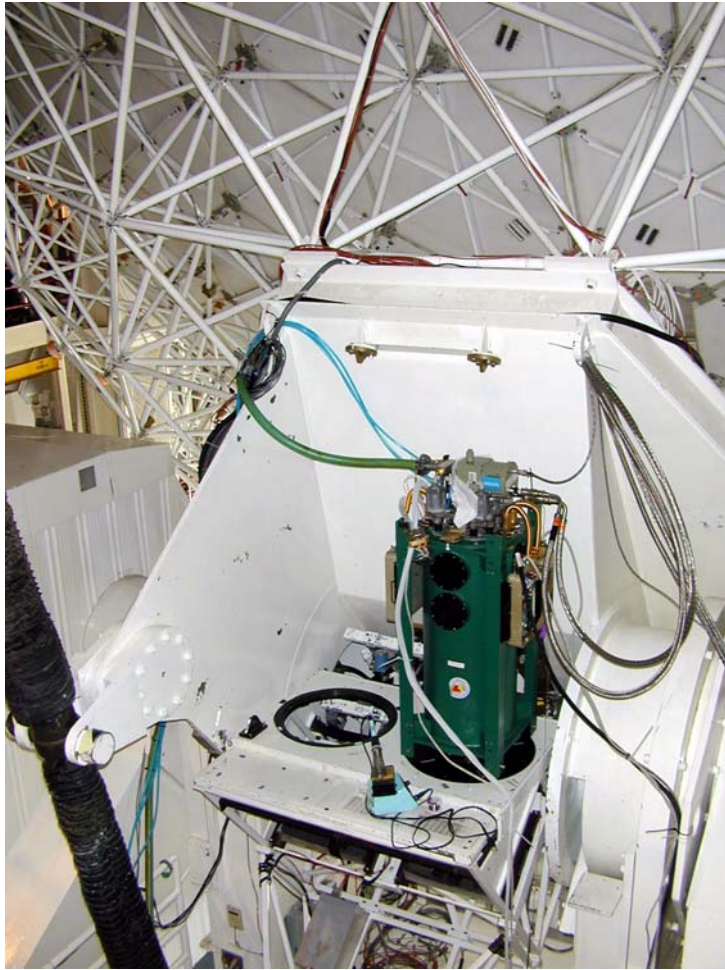


Demultiplexed readout of 8-pixel  
TES bolometer with chopped  
bolometric load



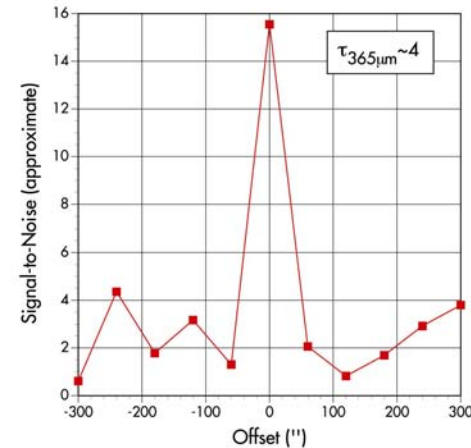
Demultiplexed signal from FIBRE while  
sweeping the Fabry-Perot (orange) across a  
local oscillator source with a spectral  
resolving power of 1200. Only one  
bolometer channel is in range. Some optical  
crosstalk evident in 'off' channels from  
Stray light.

## FIBRE: astronomical data at CSO



- *Multiplexer operated stably on telescope*
- Photon noise limited
- Dark detector NEP  $\sim 3 \times 10^{-17} \text{ W}/\sqrt{\text{Hz}}$  consistent with theoretical phonon noise.

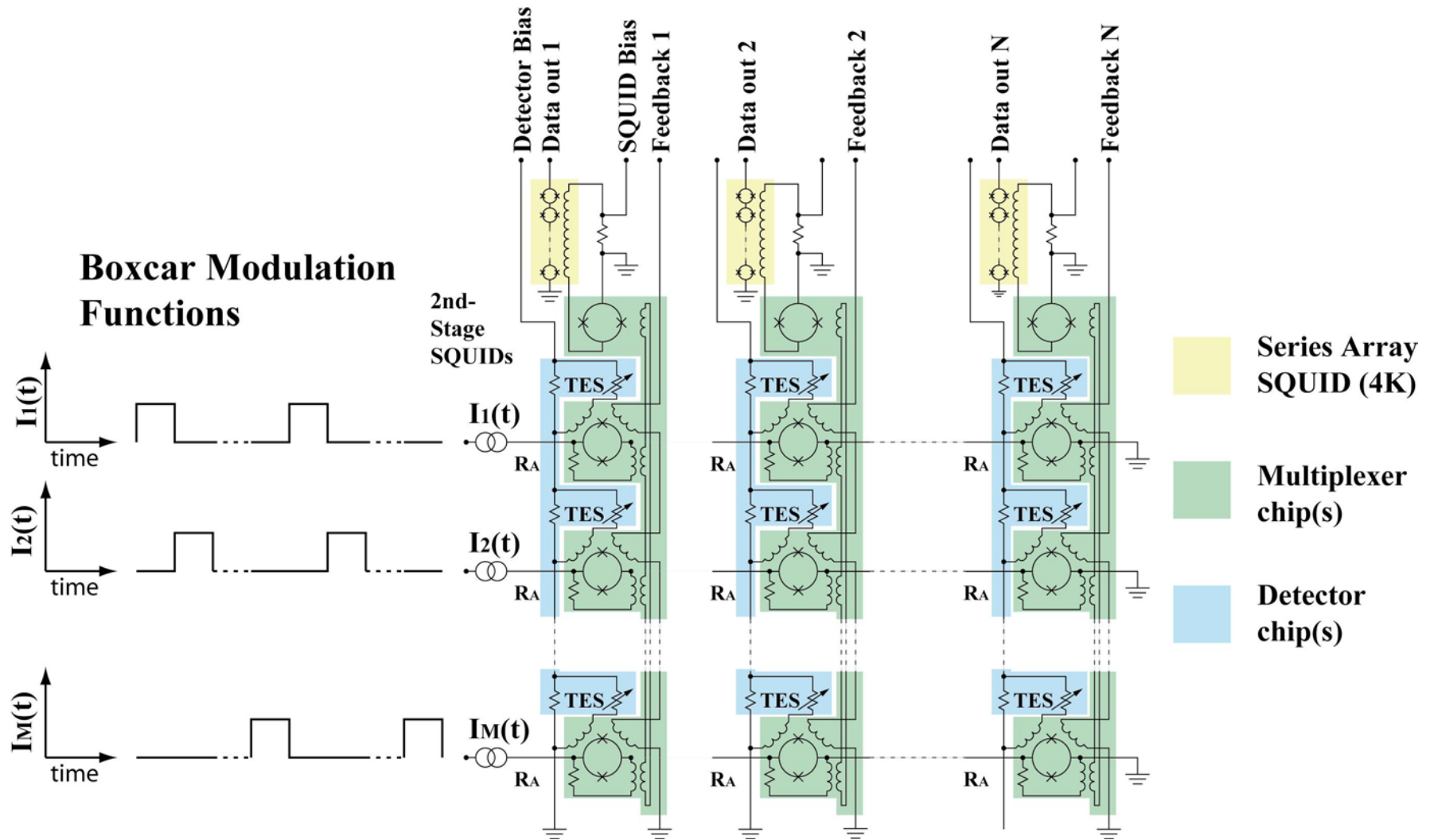
FIBRE Observation of the Moon Limb at  $365\mu\text{m}$

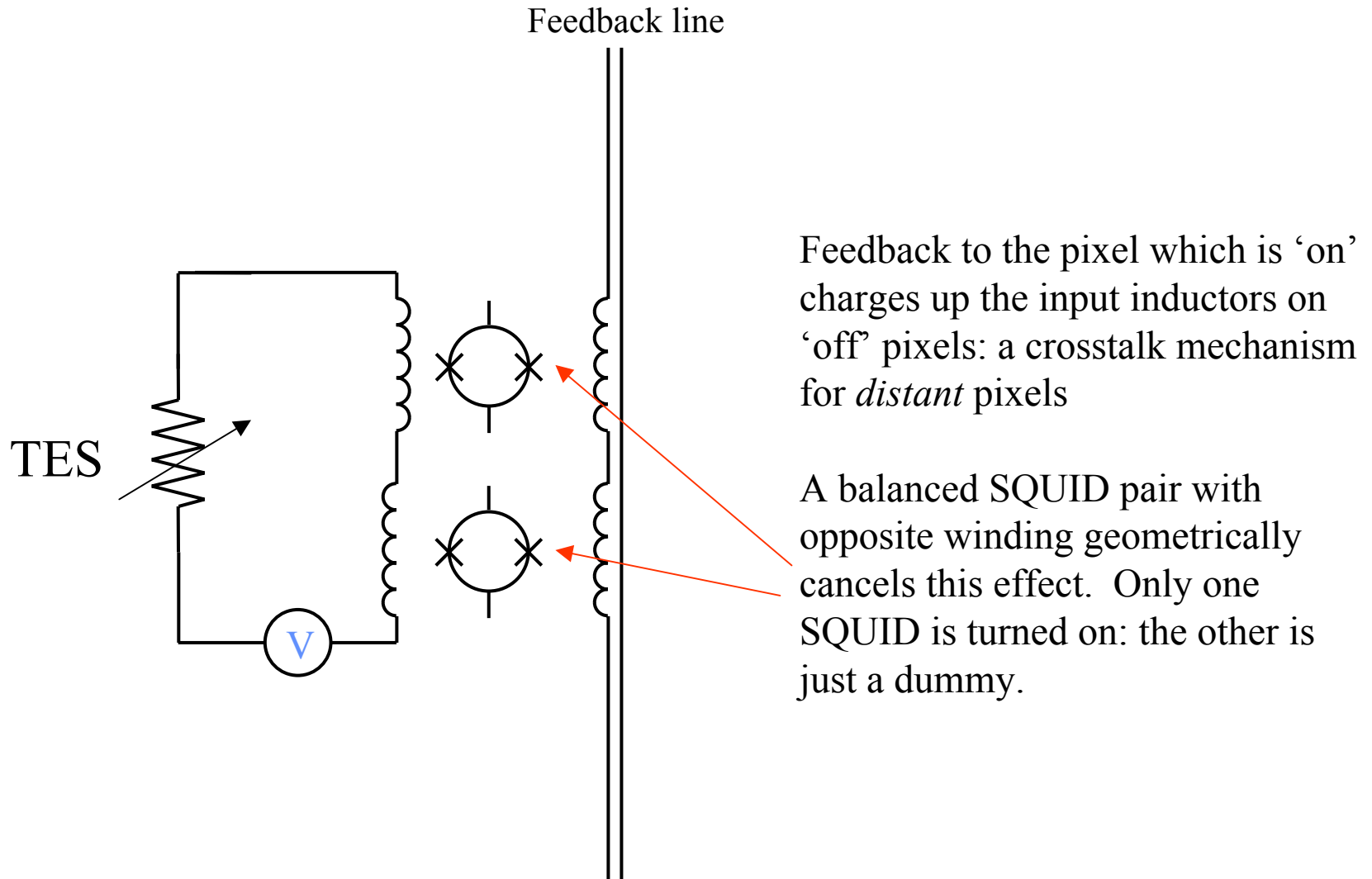


The weather was too poor during the observation window to see galactic sources, so the moon was observed at spectral resolving power of 1200.

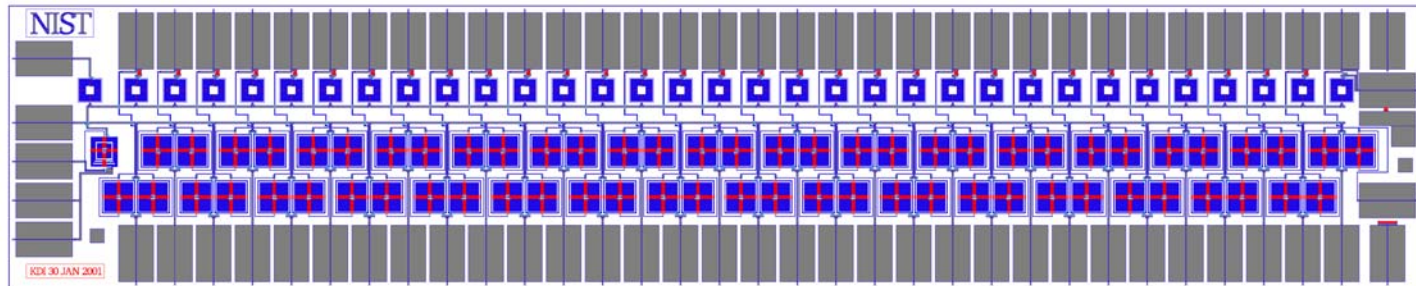


- In order to prevent parasitic currents flowing through the wrong paths in the parallel-addressing configuration, the address resistors have to be made large ( $\sim 100 \Omega$ ). This led to high address current, high power dissipation, and address-line crosstalk.
  - > series address circuit
- The coupling of the common feedback coil to the input circuits of the 'off' SQUIDs is an important crosstalk mechanism at high switching rates.
  - > eliminate feedback-input coupling with 'balanced' SQUIDs.

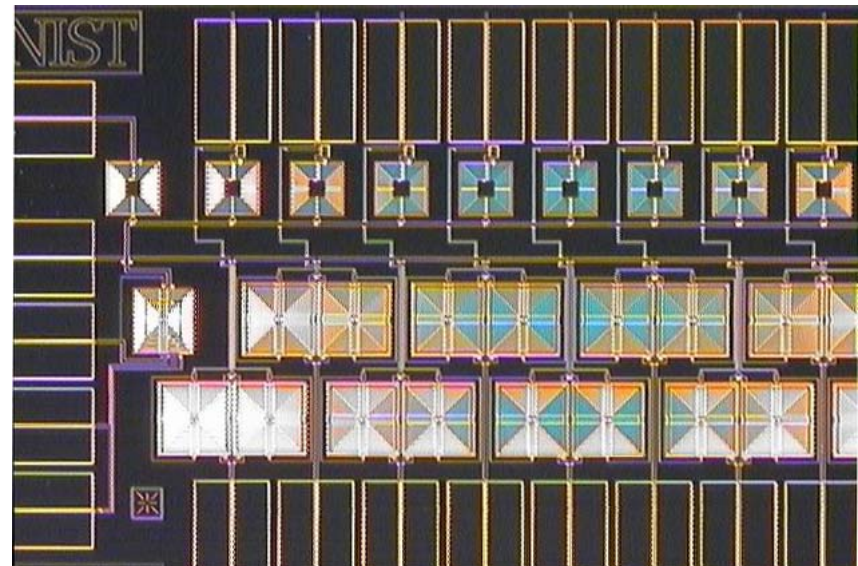


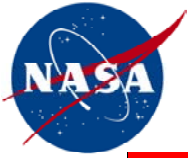






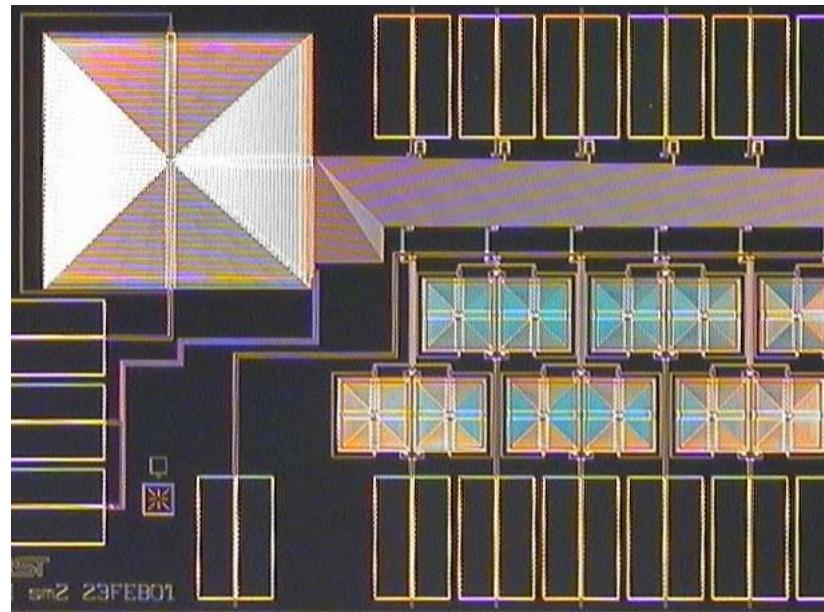
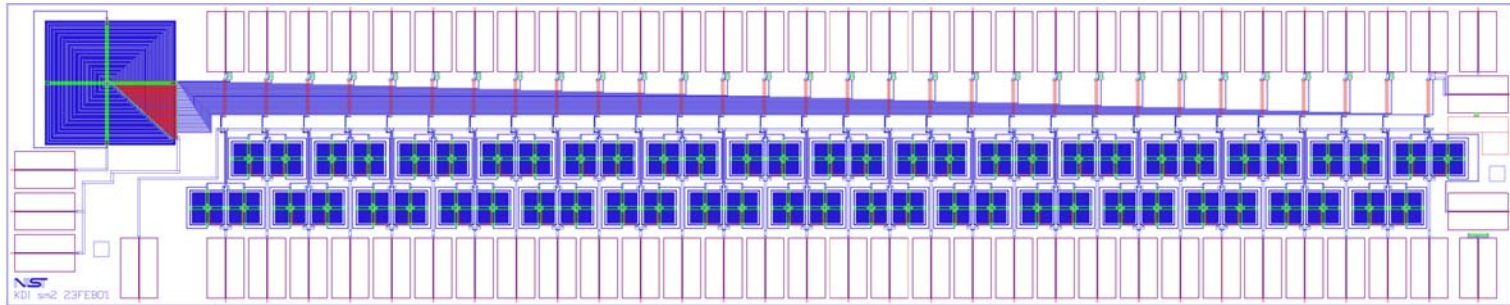
- 1x32. Need 32 chips to instrument kilopixel array.
- Series Addressing – low xtalk, low power ( $\sim 1\mu\text{W}$  for 32 x 32).
- Balanced SQUID input to zero feedback-input coupling xtalk



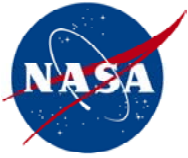


## 32 x N Multiplexer with Individually Coupled 2<sup>nd</sup> Stage

NIST

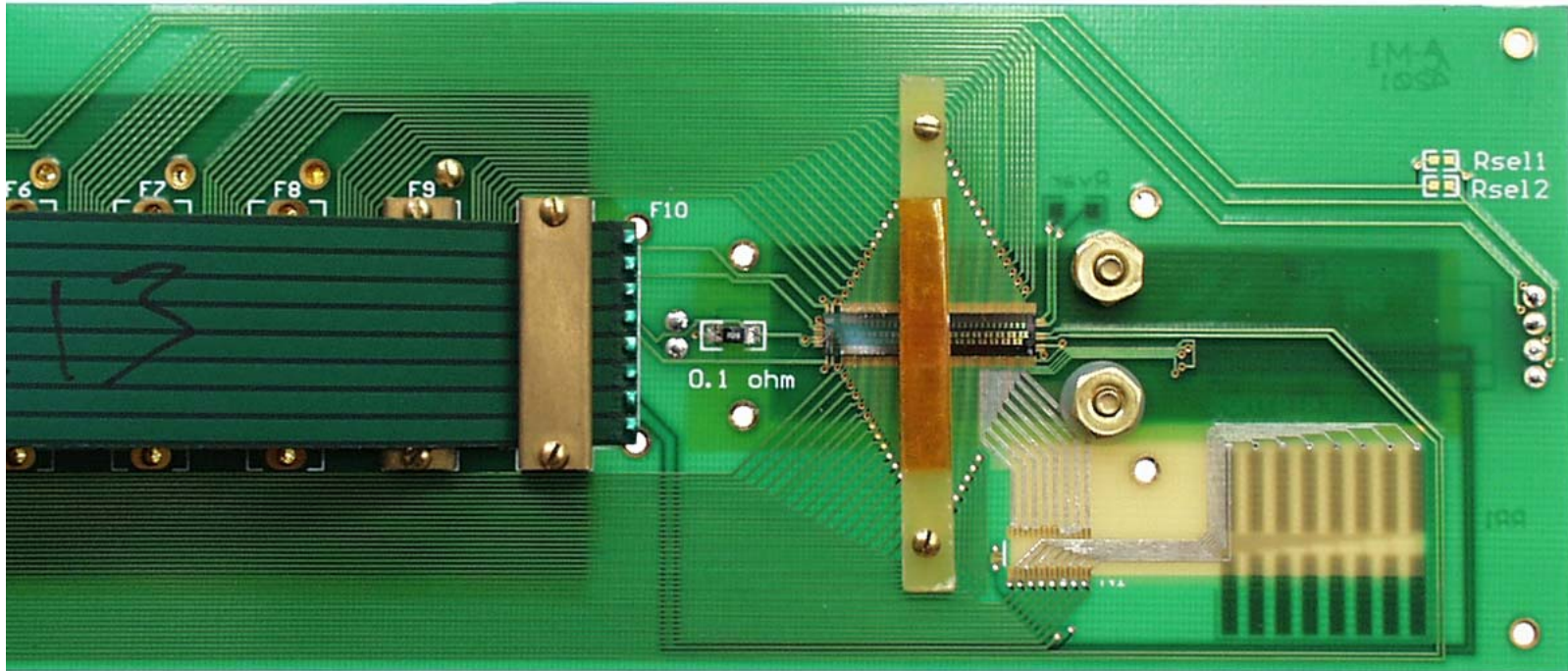


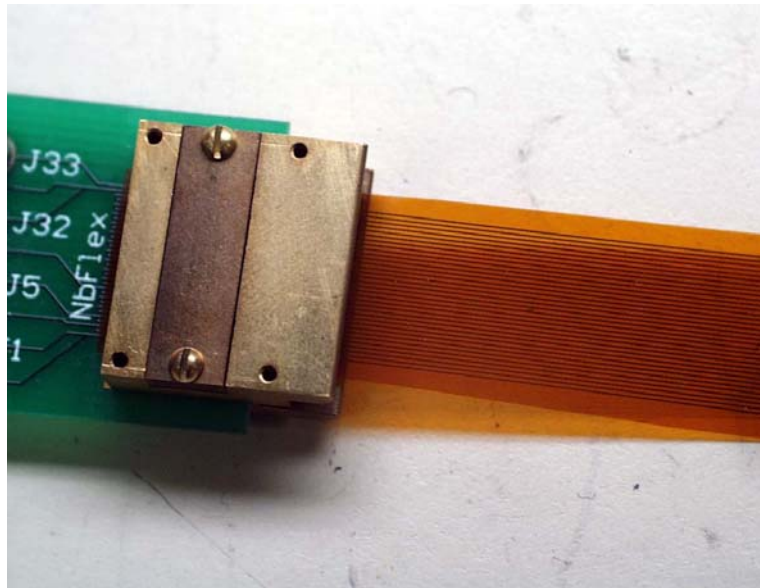
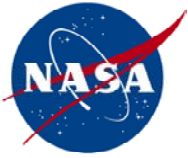




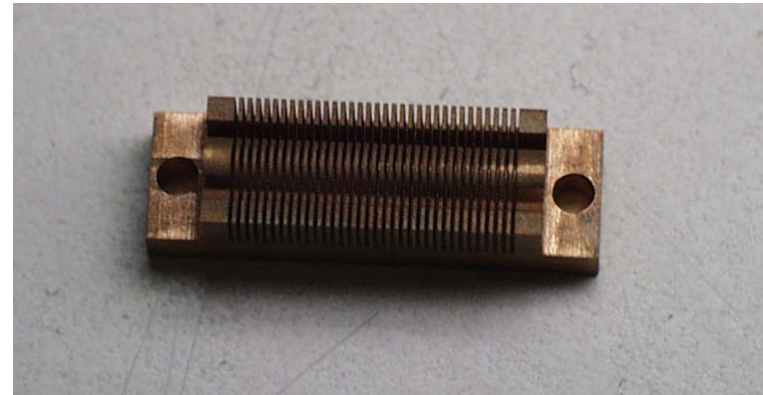
## MUX Board

NIST





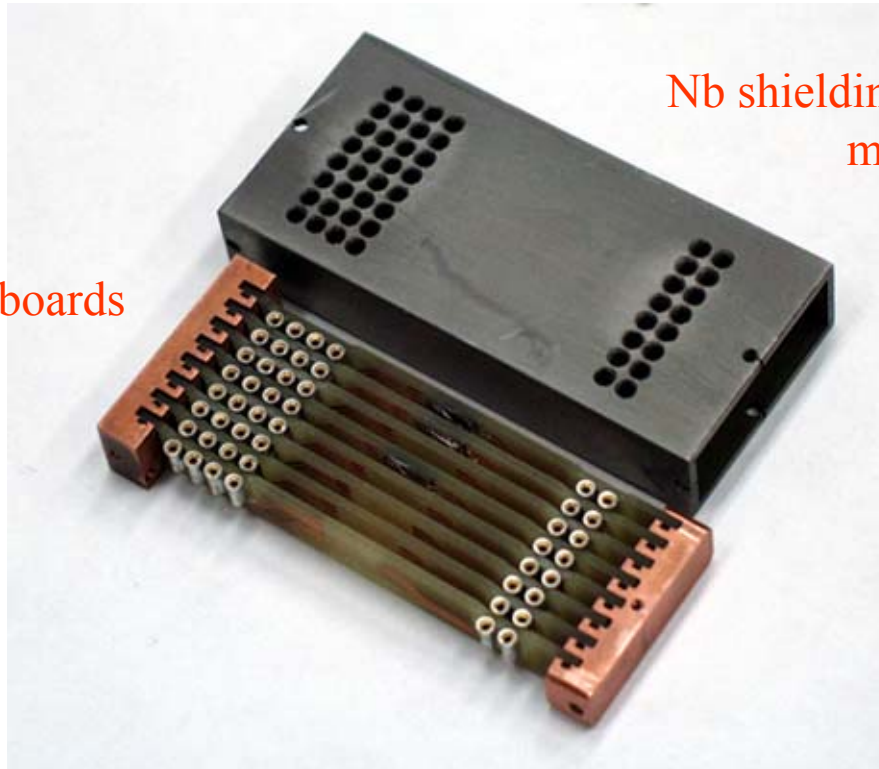
Nb Flex



Be-Cu springs for Nb flex connector



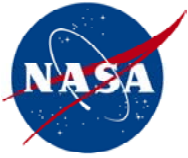
8 SQUID boards



Nb shielding outside  
mu-metal

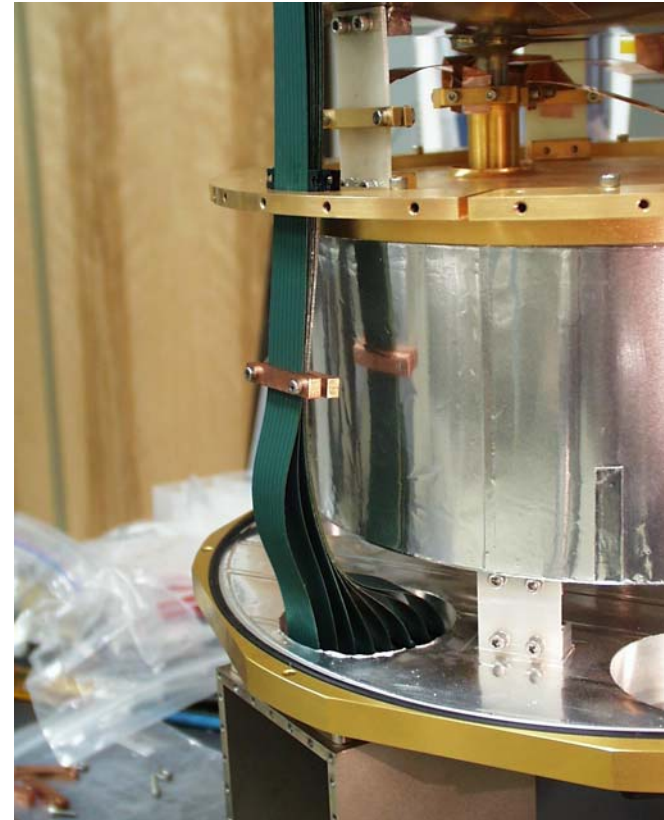
8 modules required  
for 32 x 32  
multiplexed  
array





## Cu-Ni Flex 4K - 300 K

NIST

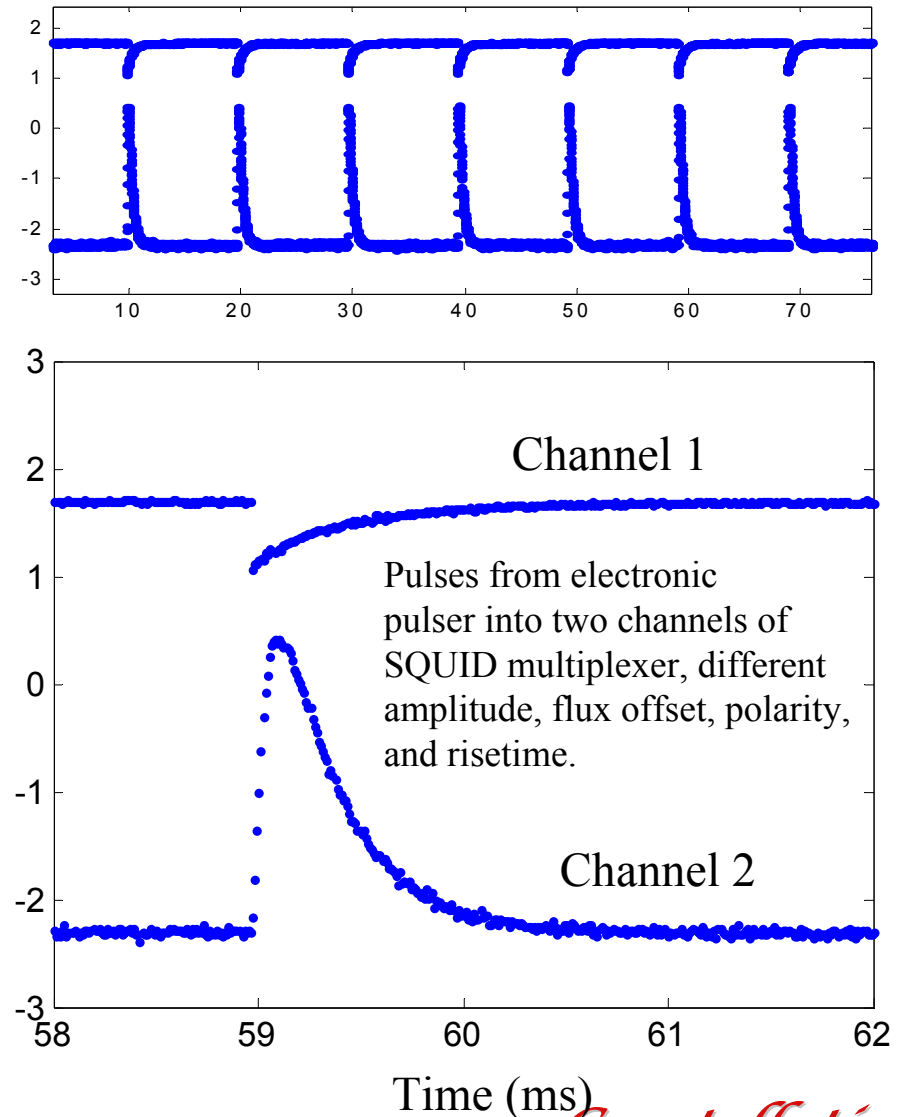


8 flex, each with 16 conductors  
(8 signal, 8 return)



Currently being tested

- Performance stable
- Noise looks good
- ~16 channels tested, all look good.
- Operation at ~500kHz demonstrated - improving
- Need to implement switched digital feedback



Time (ms)

*Constellation-X*



Nearest Neighbor:	$\sim 0.25 \%$
Next nearest neighbor:	$\sim 0.025 \%$

This does *not* include optical or thermal crosstalk, or crosstalk in the input circuit - only the crosstalk in the SQUID multiplexer itself.



## Noise aliasing

Signal band  $1/(2 \cdot \pi \cdot 100\mu\text{s}) = 1.6 \text{ kHz}$

L/R band  $\sim 10 \text{ kHz}$

Nyquist sample rate  $\sim 20 \text{ kHz}$

32 pixels  $\sim 600 \text{ kHz}$

x2 noise margin  $\sim 1.2 \text{ MHz}$

## Arrival time determination

Con-X response time goal  $\sim 100 \text{ us}$

Sample 20x on fall, 3x on rise  $\sim 5 \text{ us}$

Multiplex 32 pixels  $\sim 150 \text{ ns}$

Line Rate: 6.4 MHz